AN OVERVIEW DISCUSSION OF PROPAGATION EFFECTS OF NUCLEAR ENVIRONMENTS ON VLF-LF COMMUNICATION SYSTEMS



2495

AD A O

The Rand Corporation 1700 Main Street Santa Monica, California 90406

31 August 1975

Topical Report for Period 4 September 1974-31 August 1975

CONTRACT No. DNA 001-74-C-0019

APPROVED FOR PUBLIC RELEASE;
DISTRIBUTION UNLIMITED.

THIS WORK SPONSORED BY THE DEFENSE NUCLEAR AGENCY UNDER SUBTASK \$99QAXHE043-26.

Prepared for

Director

DEFENSE NUCLEAR AGENCY

Washington, D. C. 20305





SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)								
	(12) REPORT DOCUMENTATION	READ INSTRUCTIONS BEFORE COMPLETING FORM						
18)	I. REPORT/NUMBER	2 GOVT ACCESSION NO.	RECI. IENT'S CATALOG NUMBER					
بر:	DNA 3778T	CARTON PERFORM	5 YPE OF REPORT & PERIOD COVERED					
(AN OVERVIEW DISCUSSION OF PROPARATE OF NUCLEAR ENVIRONMENTS ON VIET	GATION EFFECTS (LF COMMUNICATION	Topical Report for Period 4 Sep 74-31 Aug 75.					
	SYSTEMS.	= 3	6 PERFORMING OPG REPORT NUMBER					
	7. AUTHOF(s)		8 CONTRACT OR GRANT NUMBER(s)					
	C. M./Crain	(15)	DNA 691-74-C-9919					
	3 PERFORMING ORGANIZATION NAME AND ADDRESS The Rand Corporation	TO DNA	NWED Subtask					
	1700 Main Street	1	\$99QAXHE043-26 F. 1943					
	Santa Monica, California 90406		12 REPORT DA'IE					
	Director Defense Nuclear Agency	(11)	31 Aug 75 13. Number of Pages					
	Washington, D.C. 20305 14 MONITORING AGENCY NAME & ADDRESS(II dillere	nt from Controlline Office)	28					
	MONITORING AGENCY NAME & ADDRESSIT ATTENT	521-	UNCLASSIFIED					
			15a DECLASSIFICATION/DOWNGRADING SCHEDULE					
	16 DISTRIBUTION STATEMENT (of this Report)							
	Approved for public release; di	ited.						
	Approved for public release, or							
	17 DISTRIBUTION STATEMENT (of the abstract entered	d in Block 20, ii dillerein ii	om Reporty					
	18 SUPPLEMENTARY NOTES							
	This work sponsored by the Defense Nuclear Agency under Subtask \$99QAXHEO43-26.							
19 KEY WORDS (Continue on reverse side if necessary and identify by block number)								
	VLF-LF Systems							
'	Nuclear Effects							
	20 SETRACT (Continue on reverse side in necessary a	ind identify by block number	oring can the general features					
	It is the purpose of this brief overview to bring con the general features of long-wavelength propagation at VLF and LF frequencies, how nuclear							
	environments can degrade the normal communications capability which these systems provide, the consequences of remaining uncertainties in predicting							
	the degree of degradation expense	cted under worst	-case conditions. More					
	detailed technical understandi	ng of the overal.	I brontem is avaitable in					
	DD FORM 1473 EDITION F 1 NOV 65 IS OBS	OLETE	AGGTRIED					
	1 JAN 73 14/3	3 119(C)	LASSIFIED ASSIFICATION OF THIS PAGE (When Date Entere					
			296 600					
			÷ · ·					

mit

TABLE OF CONTENTS

		Page
I	BACKGROUND AND INTRODUCTION	3
II	NUCLEAR EFFECTS ON AVAILABLE RADIO MEANS FOR LONG RANGE COMMUNICATIONS	7 7 7 9 10
III	OPERATIONAL DEGRADATION OF VLF-LF SYSTEMS IN NUCLEAR ENVIRONMENTS	13
τv	SUMMARY AND CONCLUSIONS	19

ACCERSION	for	V			
RTIS	White Section	1			
DOC	Beff Spotian 🔯	l			
WANTOURG		I			
JUSTIFICATI	ON III	I			
DY					
Brst.	AVAIL ARRAY SPECIAL	1			
A					

LIST OF ILLUSTRATIONS

	Page
Illustration of long-range signal transmission means	8
Illustration of hypothetical three burst modification of transmission waveguide	12
Possible signal amplitude reduction due to nuclear environment	15
Illustrative situations where nuclear environment has much different effects on received signal-to-noise ratio	17
	Illustration of hypothetical three burst modification of transmission waveguide

AN OVERVIEW DISCUSSION OF PROPAGATION EFFECTS OF NUCLEAR ENVIRONMENTS ON VLF-LF COMMUNICATION SYSTEMS

I. BACKGROUND AND INTRODUCTION

In recent years much national effort has been directed toward providing assured survivable communications from the NCA and CINCS to the various elements of the strategic forces under conditions of heavy nuclear attack. This effort has included a variety of communication means--satellites, rockets, airborne transmitters, mobile and dispersed surface facilities, and both soft and hard fixed surface facilities. Transmission frequencies of interest cover the radio frequency spectrum from a few hertz to some 10^{11} hertz. For the vital function of providing minimum essential one-way assured communication from the command authorities to the force elements, particular attention has been given to communication systems which use transmission frequencies below about 10 hertz. This is because of the attractive propagation characteristics of these so-called long wavelength radio signals. The Navy has actively pursued the development of a system (SANGUINE) employing a buried transmitter(s) which radiate signals at frequencies below 102 hertz in the so-called ELF (extremely low frequency) region of the radio spectrum. The Air Force and Navy have developed capabilities to transmit signals from both fixed and airborne transmitters in the range between 10^4 and 10^5 hertz, i.e., in the upper VLF (very low frequency) and lower LF (low frequency) portions of the radio spectrum.

A common feature of communication systems capable of long range communication at frequencies in the VLF and LF portions of the radio spectrum (the frequency region examined in this report) is that the transmitters require physically large radiating elements and high transmitter input power. For this reason it is not practical to attain long range two-way communication capabilities between command authorities and the force elements by use of these frequency bands.

Despite their being limited to one-way communication functions, the potential capability of long wavelength systems--using practical transmitter facilities and radiated powers--to provide communications at global or a sizable portion of global distances for very vital purposes has provided one of the principal bases for development of such systems.

Interest in new and physically survivable long wavelength communication systems was considerably increased in the early 1960s. This occurred because HF (high frequency, 3-30 MHz) radio communication was considered relatively more vulnerable to disruption due to effects produced by nuclear weapon detonations--particularly detonations at high altitude--than communication systems which operated in other portions of the radio spectrum. Following the 1962 high altitude tests a considerable amount of data on VLF transmission effects caused by the various high altitude bursts became available from many sources -- to a large extent from groups routinely monitoring the several world-wide VLF transmitters of the United States, the USSR, Japan, These data clearly indicated that the previously prevailing general impression that VLF transmission would not be seriously affected by nuclear burst environments was incorrect. The Defense Nuclear Agency, recognizing the importance of developing an improved understanding of VLF propagation in nuclear environments, organized a working group which met at Stanford Research Institute in October, 1963. The participants included those having relevant data, theoretical experts in nuclear phenomenology and long wave propagation, and those having system application interests and responsibilities. In brief, the working group found that the available data from the 1962 tests indicated generally more severe effects on VLF transmission than previously anticipated, that the understanding of the nuclear phenomenology and VLF propagation was inadequate to explain the observed effects, and that those using and planning systems employing VLF transmission sorely needed better information on expected system performance in various feasible nuclear environments. Shortly after the meeting of the DNA Working Group on VLF it was recognized that positive and negative ions as well as electrons could significantly influence VLF and LF propagation in a nuclear environment and that previous assessments which included only electrons were in general

optimistic; the inclusion of ion effects subsequently made possible a much better agreement between observation and predictions and, to a large extent, eliminated the mystery as to why much of the observed propagation degradation in the 1962 tests exceeded previous expectations.

In November 1963, DNA organized a working group on LF propagation in nuclear environments which met at Rand and spent a major portion of its time studying the question of the newly proposed role of ions in LF propagation. Although important elements of ion chemistry in the relevant 30 - 60 km height region were not adequately known (such as the dominant ion species, ion-neutral collision frequencies, and several reaction rates), analyses using best estimates of uncertain parameters indicated that, at the lower LF frequencies, nuclear produced environments in the 30 - 60 km height range could have disastrous consequences to normal sky-wave propagation. The major conclusion of the working group was that:

"In any event, it appears basically sound, in order to provide invulnerablility to nuclear burst-produced propagation effects, to design LF systems on the basis of a surviving groundwave signal and normally expected noise backgrounds."

The height region from 30 to 60 km has proved most difficult for experimental work on charged particle chemistry, and important uncertainties remain; however, present understanding supports the above conclusion of the LF working group.

Since it became recognized that long wavelength signal propagation could be upset to an operationally significant degree by nuclear burst environments, DNA has supported theoretical and experimental work directed toward making available to system operators and planners the needed degree of understanding for judicious system development and operational assessments. A sizable amount of information relevant to the problem has been obtained and documented in DNA handbooks and reports. This work includes theoretical work on signal propagation under normal and disturbed conditions; experimental work under natural disturbed conditions such as exi occasionally in polar regions following large solar disturbances; theoretical and experimental work directed toward resolving the major uncertainties concerning the conductivity of the lower ionosphere and, hence, the propagation characteristics of long wavelength signals; simulation of transmission path performance using models which closely resemble the earth-ionosphere transmission waveguide; and

calculated transmission effects at VLF and LF frequencies for a wide variety of assumed plausible nuclear burst environments and typical opertional path geometries. As a result, a vastly improved understanding, relative to that existing when atmospheric nuclear testing was terminated, has evolved and is available for use by system planners, operational users, war game studies, etc.

A. Long Range Radio Communications

Radio transmission of information between terminals wel! beyond lineof-sight is possible by several techniques which employ a wide range of the
radio spectrum from ELF to the millimeter wavelengths. For transmission
to distances of more than several hundreds of kilometers, three principal
means, namely long wavelength (VLF and LF) propagation, high frequency (HF)
propagation, and satellite relay are currently in operational use. All
three means are subject to deleterious propagation effects (in addition to
physical effects on terminals and terminal equipment not considered in this
report) which may be brought about by nuclear detonations. Figure 1 illustrates the more germane features of how signals are propagated from transmitters to receivers by the three methods, and also indicates for each method
the important height regions where the signal is subject to the more significant nuclear effects.

B. Satellite Relay

In the case of satellite relay transmission, the signal may be reduced in amplitude and modified in phase by excess ionization produced below about 400 km for nuclear bursts in general. This effect is a straightforward transmission phenomenon though an ionized medium. Under non-nuclear conditions it is negligible at the frequencies normally used [UHF (300-3,000 MHz) and above]. Under nuclear disturbed conditions important amplitude reduction or "black-out" effects can be produced, particularly at the lower frequencies. The more generally significant effect on satellite relay transmission under either normal or nuclear disturbed conditions is caused by large scale striated type structures which exist normally or may be induced by nuclear detonations in a region from perhaps as low as 100 km altitude to perhaps as high as several thousand km. Satellite transmission effects and their understanding is being actively studied by DNA and others (those primarily concerned with natural conditions) and is mentioned here only for purposes of perspective on the three principal long range transmission methods.

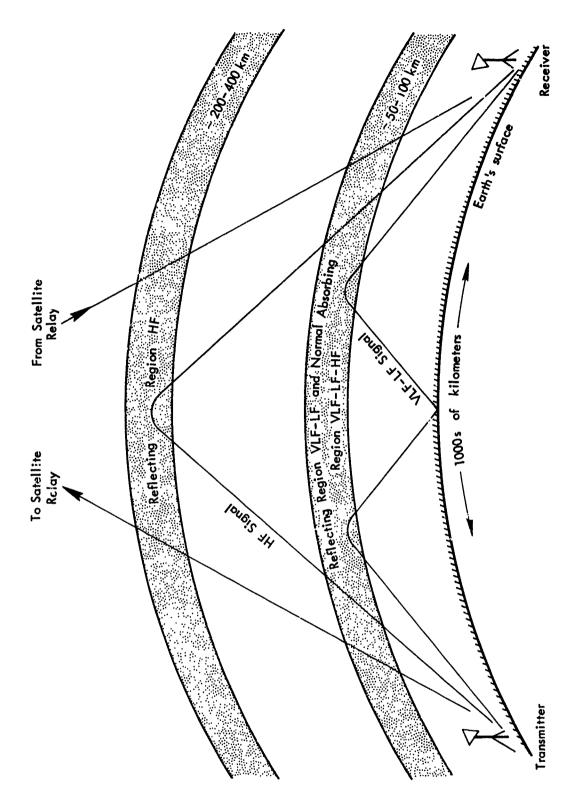


Fig. 1 —— Illustration of long-range signal transmission means (not to scale)

C. High Frequency Radio Communications

For the same reason it is worthwhile to briefly discuss HF transmission. High frequency signals propagate to large distances due to "reflection" from the upper regions of the ionosphere, typically at altitudes from 200 to 400 km depending on frequency, time of day, and geographical location. For a ionosphere reflection height of, say, 300 km transmitted signals can reach receivers up to distances of about 4000 km by means of a single ionospheric reflection. Transmission by multiple reflections between the ionosphere and earth can be efficient enough to occasionally permit useful signals to be propagated globally; however, the reliability of normal HF transmission is well under 100 percent for single ionospheric reflection and degrades appreciably with each subsequent reflection. As shown in Fig. 1, the propagated signal has to pass through the absorbing lower ionosphere before reflection by the more intensely ionized and "reflecting" upper ionosphere. Under normal daytime conditions absorption of the signal by the lower ionosphere (D region) is high enough to prevent useful long-range signal transmission at the lower HF frequencies but low enough at the higher HF frequencies (which can be reflected by the upper ionosphere) to permit useful communication. At night the upper ionosphere is less highly ionized; hence lower frequencies must be used than in the daytime in order to secure reflection. At night, ionization in the lower ionosphere (the height region of daytime absorption) almost completely disappears, and consequently the lower frequencies in the NF band can then be employed for the long-range transmission. By judicious choice of frequency for a given path and time of day, satisfactory communication can be achieved in the FF band to very long ranges both by day and by night.

Nuclear detonations can deleteriously disturb or completely disrupt HF transmission by producing added ionization at lower levels. This causes absorption in the lower ionosphere (say from 50 to 150 km). Nuclear detonations of sufficient altitude also create large mechanical disturbances which destroy the mirror-like reflecting properties of the normal ionosphere. HF frequencies are the ones most subject to deleterious propagation effects in nuclear-produced environments. Their relative vulnerability was anticipated and was demonstrated in the high altitude test programs of 1958 and

1962. Assessment of the degree of degradation of HF communication systems by nuclear bursts is highly dependent on scenarios and other assumptions. DNA has available several documents, handbooks, and reports on expected system performance in a variety of plausible nuclear environments. In general, disruption is least for nighttime conditions and for single bursts. It is greatest for multiple-burst environments and daytime conditions. Also, as suggested by Fig. 1, degradation due to absorption of the signal is only significant if the HF transmission passes through the lower ionosphere (D region) at a location where the ambient ionization has been appreciably enhanced by nuclear radiations. For single bursts, depending on height, it is possible to have situations where paths whose terminals are close to the burst-region are less upset than the paths with more remote terminals. Attempts to assess test data in terms of the proximity of the great-circle path to the burst have led to difficulty, and have caused some confusion about the degree of understanding of the HF blackout problem. It is necessary to treat the problem as three dimensional, to consider explicitly the geometry of the transmission path, and to allow for the height at which absorption is introduced. When this is done, the test data (single bursts in all cases) are in reasonable agreement with current theory.

D. Long-Wavelength Radio Communications

Propagation of long-wavelength signals to distances of the order of 1000s of kilometers is basically different from HF propagation and to propagation between satellite and earth stations. For HF and satellite communications one can reasonably consider the propagation paths to be ray; that pass through nuclear-disturbed regions of the ionosphere. For long-wave transmission, on the other hand, one can consider the signal to be guided in the waveguide formed by the conducting earth (lower boundary) and the lower conducting ion-osphere between about 60 and 90 km altitude under normal conditions. Nuclear radiations change the physical height of the upper waveguide boundary and its vertical and horizontal conductivity structures. This causes phase and amplitude changes of the signal propagated in the waveguide. Instead of thinking in terms of integrated effects along rays (illustrated in Fig. 1), which pass

through regions whose ionization content has been increased by nuclear radiations one can think of long-wavelength propagation effects as arising from distributed effects along the waveguide path. For a burst at very high altitude (say, an earth radius), the upper waveguide boundary is uniformly changed both in height and conductivity gradient along much of the propagation path. The expected change in signal phase and amplitude can then be evaluated using waveguide propagation theory by calculating the attenuation and phase shift per unit distance along the waveguide and applying these parameters to the appropriate length of path. In most plausible nucleardetonation scenarios the upper boundary of the waveguide is not uniformly modified and the problem of confidently estimating the propagation effects caused by burst(s) is much more difficult. Theoretical techniques have been developed in DNA studies for solving long-wave propagation problems for an arbitrarily non-uniform waveguide boundary such as would be produced by either single bursts at high altitude or by a number of bursts with a detonation distribution in space and time such as would be expected in real nuclear engagements. Also experimental work using scaled models has permitted checking the VLF-LF theoretical work concerning irregular waveguides. Comparisons of theory and simulator experiments have proved quite satisfactory. Figure 2 illustrates the general features of the irregular waveguide concept. The normal or undisturbed waveguide boundary is shown at constant height and can be considered to have a reasonably uniform vertical gradient of conductivity, whereas the waveguide boundary produced by the three illustrated nuclear bursts is quite variable in height and in vertical conductivity gradient along the path between transmitter and receiver. During the transition periods from night to day and day to night, the normal waveguide boundary undergoes a slow change in height and conductivity gradient in the regions of sunset and sunrise. Studies of transmission effects along paths traversing these transitional regions thus provides an additional opportunity to assess the theoretical propagation models; however as suggested by Fig. 2 the problem is much more complex for many feasible nuclear environment situations than for the single natural change of the waveguide height produced in the day-night transition region.

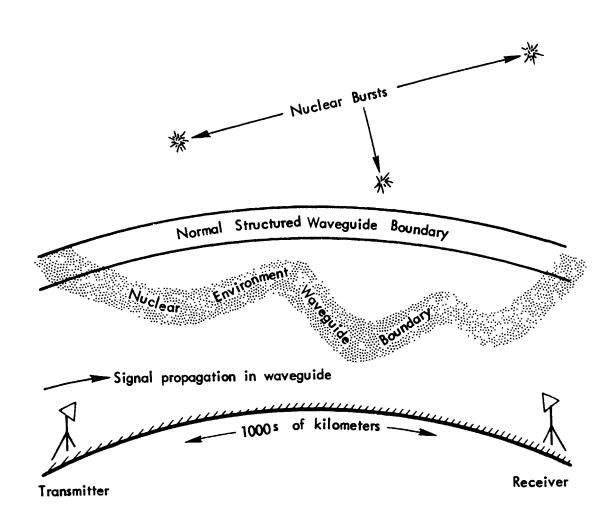


Fig. 2 — Illustration of hypothetical three burst modification of transmission waveguide (not to scale)

III. OPERATIONAL DEGRADATION OF VLF-LF SYSTEMS IN NUCLEAR ENVIRONMENTS

As discussed in Sections I and II-D, long-wavelength radio-signal transmission can be seriously degraded by changes in the structure of the lower ionosphere (below 90 km) produced by the ionizing radiation from nuclear detonations. Both the amplitude and phase of the propagated signal can be suddenly and significantly altered by one or more bursts to such a degree that useful transmission is lost. The duration and magnitude of the amplitude and phase perturbations are directly dependent on the nuclear burst conditions (yields, heights of burst, etc.), and on the geographical relationship of the bursts to the radio transmission paths. In DNA studies a sizable number of plausible nuclear environments and path geometries have been analyzed; they are documented in available DNA literature (handbooks and "aports). One should refer to this material for detailed understanding of specific situations. Current and proposed VLF-LF systems are not immune to degradation or disruption as was generally assumed prior to the in-depth investigations in recent years. While such systems may be considered relatively "survivable" compared to long-range HF communication systems for plausible nuclear environments, they are unquestionably subject to difficulties that should be known and considered by those concerned with system planning, development, and operations.

For purposes of this report the degree to which VLF-LF system performance can be affected by nuclear environments is presented in a relative way, i.e., the upper limit or worst-case degradation from possible and plausible nuclear scenarios and relevant transmission paths is referenced to the normally experienced transmission levels. In this way one can relate the current peacetime performance of VLF-LF systems as obtained from day-to-day experience to possible performance of the same systems under nuclear environment conditions. This approach illustrates how serious the degradation may be but does not provide the detailed understanding for specific links and for prescribed nuclear burst scenarios which may be obtained from the available DNA literature and computational capability. In general the performance of a VLF-LF link can lie between the normal peacetime performance and the upper

en en de la company de la comp

limit values of signal disturbance presented, depending on the nuclear-burst scenario postulated.

In order to indicate the upper limits of possible degradation in a simple way, it is necessary to adopt a simplified but adequate approach for the range of frequencies involved. One can consider the propagation between a given transmitter and receiver to occur by two separate mechanisms, namely a ground wave transmission which is independent of the lower ionosphere, and skywave transmission which is dependent primarily on the height and conductivity-profile of the lower ionosphere. This approach becomes increasingly more approximate as the frequency of transmission is lowered. Likewise, for a given frequency, the approximation gets worse as the severity of the nuclear perturbation of the ionosphere is increased. However, the principal features of expected degradation are obtained with adequate accuracy for an overview of the problem. The results obtained by separating the treatment of the ground and sky waves is likely to underestimate amplitude reduction of the propagated signal. This can be verified by comparing the results of this report with those available in the DNA literature using more precise treatments.

Figure 3 shows, as a function of distance between transmitter and receiver, the difference in signal level between the sky-wave and ground-wave components of the signal. The values plotted are for typical conducting earth parameters and for typical normal day and night ionospheric structures and are not significantly dependent, for purposes of this report, on the earth and ionosphere parameters used. To illustrate what one can determine from Fig. 3, consider a transmission path of 3000 statute mi'es and a transmission frequency of 20 kHz. It is seen that the sky wave exceeds the ground wave by 29 dB during daytime (noon) and by 24 dB at night. Under normal conditions, such as those experienced in day-to-day operations during peacetime, the signal at a receiver 3000 statute miles from a transmitter is that provided by sky-wave propagation. If a severe nuclear environment is created along the path between the transmitter and receiver resulting in complete loss of the sky wave, one would receive a signal due to ground-wave propagation which is 29 dB (day) or 24 dB (night) lower in amplitude.

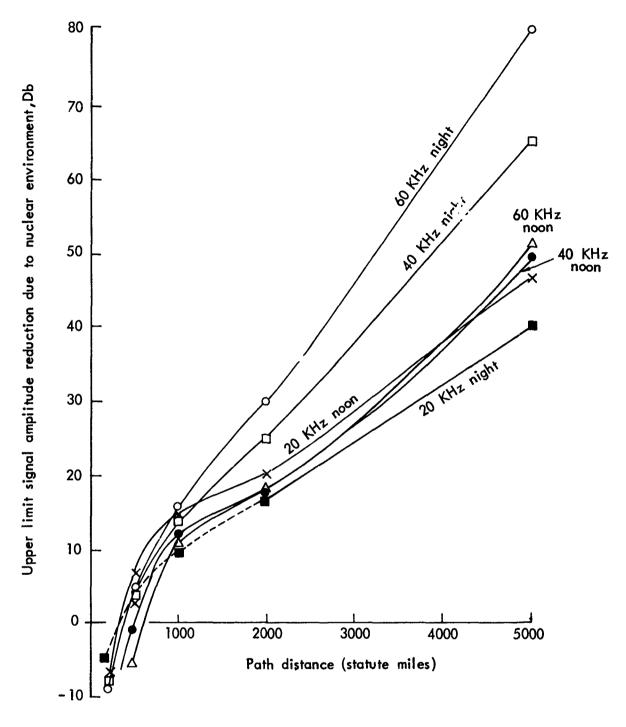
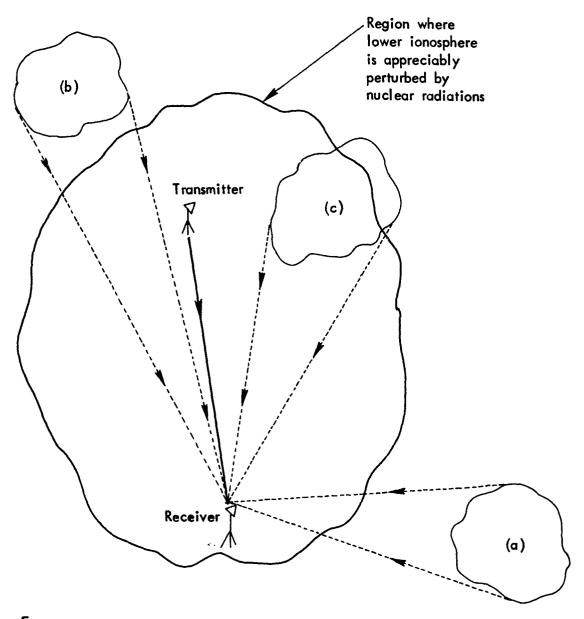


Fig. 3 — Possible signal amplitude reduction due to nuclear environment

Accompanying the amplitude reduction would be a very large change in signal phase, with time characteristics determined by the rate at which the lower ionospheric structure was modified by the nuclear radiations. The fastest rate of change of signal phase would occur for a large single burst at high enough altitude to illuminate the entire path at the same time. Under such conditions, phase changes of the order of a thousand degrees would occur in times of the order of a millisecond. For other burst scenarios, one can expect phase perturbations intermediate between this value and the few degrees per minute which occur naturally.

As another illustration of the use of the results of Fig. 3, consider a system which has the capability to operate in the frequency range 20 to 60 kHz and for which the operator can choose from time-to-time the frequency which provides the best communication capability at a desired distance. Results would depend on propagation conditions, ambient noise levels, and system parameters such as the dependence of effective radiated power on frequency. However, for various distances from 1000 to 5000 statute miles one could expect to use the full range of frequencies at one time or another to achieve most effective communications. At a communication range of 2000 statute miles, for example, it might turn out that 40 kHz is favorable at night and that the received signal is about 10 dB above processed noise under normal conditions. From Fig. 3 one can ascertain that, for worst-case nuclear environment conditions along the path, the signal could drop 25 dB, that is, 15 dB below noise. This assumes that the nuclear environment has no effect on noise level, which depends on whether (1) the dominant noise is from atmospherics at great distance with the propagation paths from the noise sources to the receiver passing through the nuclear perturbed region, or (2) the dominant noise source is nearby atmospheric and/or "man-made" noise. In (2) there would be negligible noise reduction and the signalto-noise would decrease by the amount of signal reduction. In (1) variation from negligible noise reduction to a noise reduction even greater than the signal reduction is to be expected depending on geographical and geometrical factors. Figure 4 illustrates three geographical situations in which the dominant source of receiver noise is distant atmospherics and in which the nuclear perturbed region has (a) negligible effect on noise level. (b) greater reduction in noise level than signal level, and (c) similar dB



(a), (b), (c), illustrate three possible regions which contribute dominant noise to receiver as discussed in text

Fig. 4 — Illustrative situations where nuclear environment has much different effects on received signal-to-noise ratio

reductions in signal and noise, depending on the geometrical relation of the noise propagation path and the region disturbed by nuclear radiation. Clearly any of the three cases, (a), (b), or (c), is possible in general nuclear engagements and for arbitrary transmission paths. Thus, in general, when the receiver noise level is dominated by distant atmospherics, communication service probability can improve or be reduced by an amount determined by the possible signal degradation levels given in Fig. 3. On the other hand, when the receiver noise level is dominated by nearby noise sources, such as is commonly the situation, reduction in signal-to-noise can be expected to be as high as indicated in Fig. 3. Maximum impact on communication service probability so far as signal amplitude is concerned can be determined for a given system and conditions (path length, frequency, etc.) using signal amplitude reduction values illustrated for 20, 40, and 60 kHz in Fig. 3. Again, one must expect large and very rapid phase variations (discussed previously on p. 16) to be associated with the reduction of signal amplitude. Generalization concerning the overall impact of signal reduction and the associated large and rapid phase changes is not possible since such impact is dependent on specific system design. It is quite feasible to provide system test signals for input to system receivers which simulate those expected to be received in nuclear environments. Using such signals for dynamic tests one can realistically assess the degree of vulnerability of the system to propagation degradation created by plausible nuclear environ-DNA can provide technical information on the magnitude and time characteristics of expected perturbations for prescribed bursts and transmission paths for such system proof tests or related user applications.

IV. SUMMARY AND CONCLUSIONS

VLF and LF long-path transmissions are subject to amplitude degradation relative to transmissions experienced in normal operations. These degradations can approximate those illustrated in Fig. 3. In addition, the amplitude reductions will be accompanied by very large (the order of a thousand degrees) and rapid (in the order of milliseconds) phase perturbations relative to those experienced in normal day-to-day operation.

Received signal and noise can be influenced quite differently depending on transmission path geometry relative to the nuclear disturbed region(s) and the location(s) of dominant noise sources and their transmission path(s) to the receiver(s) relative to the nuclear disturbances. It is possible for communication capability to increase if the nuclear perturbed region is located such as to attenuate transmission from the dominant noise sources more than signal transmission.

Capability to determine the expected signal amplitude and phase perturbations for specified nuclear scenarios and transmission paths has been developed and can be provided by DNA. Results for several postulated scenarios have been documented, and results for any other scenarios of particular user interest can be obtained and provided to the user.

System effects of the amplitude and very rapid phase perturbations possible in plausible nuclear environments can be tested by providing simulated signals for these environments to the inputs of system receivers. Such tests appear highly desirable to ascertain the degree of system survivability to be expected and/or to uncover any unexpected vulnerabilities.

DISTRIBUTION LIST

DEPARTMENT OF DEFENSE

Director

Defense Advanced Research Project Agency

ATTN: Strategic Tech. Office

Defense Communication Engineer Center

ATTN: Code R-410, W. D DeHart ATTN: Code R-820, R. L. Crawford

Defense Communications Agency

ATTN: NMCSTS, G. C. Jones ATTN: Code 480

ATTN: Code 980

Defense Documentation Center

12 cy ATTN: TC

Director

Defense Intelligence Agency

ATTN: DT-1B ATTN: W. Wittig, DC-7D

Director

Defense Nuclear Agency

ATTN: STSI, Archives

ATTN: DDST

ATTN: STVL

2 cy ATTN: STTL, Tech. Lib.

3 cy ATTN: RAAE

Director of Defense Research & Engineering

Department of Defense

ATTN: AD/DS

ATTN: DD/S&SS, John B. Walsh

Commander

Field Command

Defense Nuclear Agency

ATTN: FCPR

Director

Interservice Nuclear Weapons School

ATTN: Doc. Con.

Director

Joint Strategic Target Planning Staff, JCS

ATTN: JLTW-2 ATTN: JPST, Major J. S. Green ATTN: JPST, G.D. Burton

Chief

Livermore Division, Field Command, DNA

Lawrence Livermore Laboratory

ATTN FCPRL

Commander

National Military Command System Support Center

ATTN: DP Director for CSPO

ATTN: B-211

Director

National Security Agency

ATTN: Frank Leonard

ATTN. W-14, Pat Clark

DEPARTMENT OF DEFENSE (Continued)

OJCS/J-3

ATTN: J-3, Ops. Anal. Br., Mr. Toma

OJCS/J-6

ATTN: J-6

Director

Telecommunications & Command & Control System

ATTN: Dep. Asst., Sec. Sys. ATTN: Asst. Dir., Info. & Space Sys.

Weapons Systems Evaluation Group

ATTN: Doc. Con.

DEPARTMENT OF THE ARMY

Ballistic Missile Defense Advanced Technical Center

ATTN: ATC-T, Melvin T. Capps

ATTN: CRDABH-O, W. Davies

Manager

Ballistic Missile Defense Program Office

ATTN: DACS-BMM

ATTN: DACS-BMS, Julian Davidson

ATTN: John Shea

Commander

Harry Diamond Laboratories

ATTN: AMXDO-NP, Francis N. Wimenitz

ATTN: AMXDO-RBI, Robert Williams

2 cy ATTN: AMXDO-NP

Commander

TRASANA

ATTN: EAB

Director

U.S. Army Ballistic Research Laboratories

ATTN: AMXBR-CA, Franklin E. Niles

U.S. Army Communications Command

C-E Services Division ATTN: CEAO

Commander

U.S. Army Electronics Command

ATTN: AMSEL-PL-ENV, Hans A. Bomke

Commander

U.S. Army Materiel Command
ATTN: AMCRD-WN-RE, John F. Corrigan

Commander

U.S. Army Materiel Command

ATTN: R. Jones

ATTN: P. A. Crowley

U.S. Army Missile Command

ATTN: AMSMI-XS, Chief Scientist

ATTN. AMSMI-YTT, W. G. Preussel, Jr.

ATTN: Chief, Doc. Section

DEPARTMENT OF THE ARMY (Continued)

Commander

U.S. Army Nuclear Agency

ATTN: USANUA-W, J. Berberet

DEPARTMENT OF THE NAVY

Chief of Naval Research

Navy Department

ATTN: Code 464, Thomas P. Quinn

ATTN: Code 464, Jacob L. Warner

Commander

Naval Air Systems Command

ATTN: AIR 5381

Commander

Naval Electronic Systems Command

ATTN: PME 117

ATTN: NAVALEX 034, T. Barry Hughes

ATTN: PML 117-T, Satellite Comm. Project Off.

ATTN: John E. DonCarlos

Commander

Naval Electronics Laboratory Center

ATTN: Code 0230, C. Baggett 3 cy ATTN: Code 2200, Verne E. Hildebrand ATTN: William F. Moler

ATTN: R. Eastman

Commanding Officer

Naval Intelligence Support Center

ATTN: Mr. Dubbin, STIC 12

Naval Research Laboratory

ATTN: Hdq. Comm. Dir., Bruce Wald ATTN: Code 7750, Timothy P. Coffey

ATTN: Code 7720, Edgar A. McClean

S cy ATTN: Code 7701, Jack D. Brown

ATTN: Code 5460, Radio Propagation Br. ATTN: Code 2027, Tech. Lib.

Commander

Naval Space Surveillance System ATTN: CAPT J. H. Burton

Commander

Naval Surface Weapons Center

ATTN: Code WA-501, Navy Nuc. Prgms. Off. ATTN: Code WX-21, Tech. Lib.

Director

Strategic Systems Project Office

ATTN: NSP-2141

ATTN: NSP-27231, Marcus Meserole

DEPARTMENT OF THE AIR FORCE

Commander

ADC/AD

ATTN: ADDA

AF Cambridge Research Laboratories, AFSC

ATTN: OPR

ATTN: LI

ATTN: OPR, Hervey P. Gauvin
ATTN: LIR, T. J. Elkins
5 cy ATTN: LKB, Kenneth S W. Champion
6 cy ATTN: OPR, James C. Ulwick

DEPARTMENT OF THE AIR FORCE (Continued)

AF Weapons Laboratory, AFSC

ATTN: SAS, John M. Kamm ATTN: CA, Arthur H. Guenther ATTN: SUL

AFTAC

ATTN: TF, Maj E. Hines ATTN: TF, Maj Wiley ATTN: TN

Air Force Avionics Laboratory, AFSC

ATTN: AFAL, AVWE, Wade T. Hunt

Assistant Chief of Staff

Studies & Analysis

ATTN: Lt Col A. D. Dayton

Headquarters

Readquarters
Electronic Systems Division, AFSC
ATTN: YSEV, Lt Col David C. Sparks
ATTN: XRE, Lt Michaels
ATTN: Lt Col J. Morin, CDEF XRC

Commander

Foreign Technology Division, AFSC

ATTN: TD-BTA, Library

HQUSAF/RD

ATTN: RDQ

Commander Rome Air Development Center, AFSC

ATTN: V. Coyne

ATTN: EMTLD, Doc. Library

SAMSO/MN

ATTN: MNX

SAMSO/SZ

ATTN: SZJ, Maj Lawrence Doan

Commander in Chief

Strategic Air Command

ATTN: XPFS, Maj Brian G. Stephan

ENERGY RESEARCH & DEVELOPMENT ADMINISTRATION

EG&G, Inc.

Los Alamos Division

ATTN: J. H. M. Fu

ATTN: James R. Breedlove ATTN: James L. Walker

University of California

Lawrence Livermore Laboratory

ATTN: Terry R. Donich

ATTN: Tech. Info. Dept., L-3

Los Alamos Scientific Laboratory

ATTN: Doc. Con. for R. F. Taschek ATTN: Doc. Con. for Eric Jones

ATTN: Doc. Con. for Herman Hoerlin

ATTN: Doc. Con. for John S. Malik

ENERGY RESEARCH & DEVELOPMENT ADMINISTPATION (Continued)

Sandia Laboratories

ATTN: Doc. Con. for 3141, Sandia Rpt. Coll., ATTN. Doc. Con. for W. D., Brown

ATTN: Doc. Con. for Clarence R. Mehl, Org. 5230

ATTN: Doc. Con. for J. P. Martin, Org. 1732

ATTN: Doc. Con. for Charles Williams

ATTN: Doc. Con. for A. Dean Thornbrough

ATTN: Doc. Con. for D. A. Dahlgren, Org. 1722 ATTN: Doc. Con. for J. C. Eckhardt, Org. 1250

OTHER GOVERNMENT AGENCIES

Department of Commerce

National Oceanic & Atmospheric Admin.

ATTN: C. L. Rufenach

ATTN: Joseph H Pope

ATTN: R-43, Donald J. Williams

Department of Commerce

Office of Telecommunications

ATTN: Glenn Falcon

ATTN: G. Reed ATTN: William F. Utlaut

ATTN: L. A. Berry

Department of Transportation

ATTN: "er G. Harowles

ATTN: Code 750, T. Golden

DEPARTMENT OF DEFENSE CONTRACTORS

Aeronomy Corporation

ATTN: S. A. Bowhill

Aeronutronic Ford Corporation

ATTN: J. T. Mattingly, M.S. X-22

Aerospace Corporation

ATTN: Wallis Grabowsky

ATTN: G. W. Anderson

ATTN. T. M. Salmı

ATTN: SMFA for PWW

ATTN. V. Josephson

ATTN. S. P Bower

Analytical System's Engineering Corp.

ATTN: Radio Sciences

Avco-Everett Research Laboratory, Inc.

ATTN: Richard M. Patrick

ATTN: Guy Weyl

The Boeing Company

ATTN: D. Murray

ATTN: Glen Keister

Brown Engineering Company, Inc.

ATTN: N. Passino

ATTN, David L. Lambert, M.S. 18

University of California at San Diego ATTN: Henry G. Booker

Calspan Corporation

ATTN: Romeo A. Deliberis

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

Computer Sciences Corporation

ATTN: Barbara F. Adams ATTN: H. Blank

Comsat Laboratories

ATTN: R. R. Taur

Cornell University

Department of Electrical Engineering

ATTN: D. T. Farley, Jr.

ESL, Inc.

ATTN: J. Roberts

ATTN: R. K. Stevens ATTN: James Marshall

ATTN: V. L. Mower

General Electric Company

Space Division

ATTN: M. H. Bortner, Space Sci. Lab. ATTN: Robert H. Edsall

General Electric Company

TEMPO-Certer for Advanced Studies

ATTN: DASIAC

General Electric Company

ATTN: George H. Millman ATTN: F. A. Reibert

General Research Corporation

ATTN: John Ise, Jr.
ATTN: Peter Redmond

ATTN. John Boys

Geophysical Institute

ATTN: Tech. Lib. ATTN: Neil Brown

ATTN: T. N. Davis

GTE Sylvania, Inc.

ATTN. Marshal Cross

HRB-Singer, Inc.

ATTN. Larry Feathers

ATTN: Donald Hansen

University of Illinois

ATTN: K. C. Yeh

Information Science, Inc.

ATTN. Walter F. Dudziak

Institute for Defense Analyses

ATTN: Ernest Bauer

ATTN: Joel Bengston

ATTN: Hans Wolfhard

ATTN: J. M. Aein

International Telephone & Telegraph Corporation

ATTN Tech. Lib.

IRT Corporation

ATTN: E. De Plomb

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

ITT Electro-Physics Laboratories, Inc. ATTN: John M. Kelso

Johns Hopkins University
ATTN: Document Librarian

Kaman Sciences Corporation ATTN: F. G. Foxwell

Lockheed Missiles & Space Co. Inc. ATTN: Dept. 60-12

Lockheed Missiles & Space Company
ATTN: Billy M. McCormac, Dept. 52-14

ATTN: Robert H. Au
ATTN: Martin Walt, Dept. 52-10
ATTN: Richard G. Johnson, Dept. 52-12

M I.1. Lincoln Laboratory
ATTN: Lib. A-082 for David M. Towle
ATTN: D. Clark
ATTN: Mr. Walden, X-113
ATTN: J. V. Evans
ATTN: James H. Pannell, L-246

Martin Marietta Aerospace Orlando Division ATTN: Roy W. Heffner

Martin Marietta Corporation Denver Division ATTN: Special Projects Program 248

Maxwell Laboratories, Inc. ATTN: Victor Fargo ATTN: A. J. Shannon ATTN: A. N. Rostocker

McDonnell Douglas Corporation ATTN: N. Harris ATTN: J. Moule ATTN: Robert W. Halprin

Mission Research Corporation
ATTN: Dave Sowle
ATTN: Gary McCarter
ATTN: R. Bogusch
ATTN: Raiph killb
ATTN: R. E. Rosenthal
ATTN: P. Fischer
ATTN: R. Hendrick
ATTN: Conrad L. Longmire
ATTN: M. Scheibe

The Mitre Corporation
ATTN: Chief Scientist, W. Sen
ATTN: D. Pledger
ATTN: S. A. Morin
ATTN: G. Harding

The Mitre Corporation
ATTN: Bill Mehuron
ATTN: Allen Schneider

North Carolina State University at Raleigh ATTN: Sec. Officer for Walter A. Flood

Pacific-Sierra Research Corp. ATTN: E. C. Field, Jr.

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

Photometrics, Inc.
ATTN: Irving L. Kofsky

Physical Dynamics, Inc. ATTN: A. Thompson

The Trustees of Princeton University
ATTN: F. W. Perkins, Plasma Physics Lab.

R & D Associates
ATTN: Robert E. LeLevier
ATTN: R. P. Turco
ATTN: Richard Latter
ATTN: H. A. Ory
ATTN: William B. Wright, Jr.
3 cy ATTN: Forest Gilmore

The Rand Corporation ATTN: Cullen Crain

Raytheon Company ATTN: G. D. Thome

RCA Corporation Government & Commercial Systems ATTN: R. D. Bachinsky ATTN: Tech, Lib,

Riverside Research Institute ATTN: R. Popolow

Science Applications, Inc.
ATTN: William M. Layson

Science Applications, Inc.
ATTN: Lewis M. Linson
ATTN: D. Sachs
ATTN: E. A. Straker
ATTN: Robert W. Lowen

Space Data Corporation
ATTN: Edward F. Allen

Stanford Research Institute
ATTN: Robert S. Leonard
ATTN: Ray L. Leadabrand
ATTN: E. J. Fremouw
ATTN: L. L. Cobb
ATTN: Donald Neilson
ATTN: Charles L. Rino
ATTN: David A. Johnson
ATTN: Walter G. Chestnut

Stanford Research Institute ATTN: Dale H. Davis

System Development Corporation ATTN. E. G. Meyer

Technology International Corporation ATTN: W. P. Boquist

Thiokol Chemical Corp. Astro Met Site ATTN: G. C. Alford

Tri-Com, Inc. ATTN: Darrel Murray

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

DEPARTMENT OF DEFENSE CONTRACTORS (Continued)

TRW Systems Group
ATTN: P. H. Katscs
ATTN: J., W. Lowry

VisiDyne, Inc. ATTN: J. W. Carpenter